A Blueprint for Physically-Based Modeling of Uncertain Hydrological Systems

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We present a new methodological scheme for building physically-Abstract. 3 based models of uncertain hydrological systems, thereby unifying hydrolog-4 ical modeling and uncertainty assessment. This scheme accounts for uncer-5 tainty by shifting from one to many applications of the selected hydrolog-6 ical model, thus formalizing what is done by several procedures for uncer-7 tainty estimation. We introduce a probability based theory to support the 8 new blueprint and to ensure that uncertainty is efficiently and objectively 9 represented. We discuss the related assumptions in detail, as well as the open 10 research questions. We also show that the new blueprint includes as special 11 cases the uncertainty assessment methods that are more frequently used in 12 hydrology. The theoretical framework is illustrated by presenting a real-world 13 application. In our opinion, the new blueprint could contribute to setting up 14 the basis for a unified theory of uncertainty assessment in hydrology. 15

1. Introduction

Physically-based modeling has been a major focus for hydrologists for four decades al-16 ready. In fact, more than forty years passed since *Freeze and Harlan* [1969] proposed their 17 "physically-based digitally simulated hydrologic response model". An excellent review of 18 the related research activity during the following thirty years was presented by *Beven* 19 [2002]. Perhaps the most known physically-based model in hydrology is the Système Hy-20 drologique Européen (SHE, see Abbot et al. [1986]), which has been the subject of many 21 contributions. In the past ten years, physically-based modeling has been one of the targets 22 of the well known "Prediction in Ungauged Basins" (PUB; see Kundzewicz [2007]) ini-23 tiative of the International Association of Hydrological Sciences (IAHS). However, during 24 the last four decades it became increasingly clear that uncertainty inherent to hydrologi-25 cal processes may make the use of a deterministic model inappropriate (see, for instance, 26 Grayson et al. [1992]; Beven [1989, 2001]). 27

In fact, parallel research activity has shown the prominent role of uncertainty in hy-28 drological modeling. Some authors expressed their belief that uncertainty in hydrology is 29 epistemic and therefore can be in principle eliminated through a more accurate physical 30 representation of the related processes [Sivapalan et al., 2003]. However, recent contri-31 butions suggested that uncertainty is unavoidable in hydrology, originating from natural 32 variability and inherent randomness (see, for instance, Montanari et al. [2009]; Kout-33 soyiannis [2010]). As a matter of fact, the presence of uncertainty makes the use of 34 deterministic models impossible. 35

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Given that traditionally physically-based models are built through deterministic equations, the above emerging limitations of deterministic models may induce one to conclude that fully physically-based models are not a feasible target in hydrology, because of their incapability to deal with uncertainty [*Beven*, 2002]). Therefore two relevant questions can be raised: is it possible to cope with uncertainty while retaining a physically-based approach? And, is it possible to perform physically-based hydrological modeling and uncertainty assessment within a unified theoretical framework?

We argue that the reply to both questions above is "Yes". In agreement with *Beven* [2002], we believe that a new blueprint should be established to overcome the incapability of traditional physically-based models to cope with uncertainty. We propose that the new blueprint is built on a key concept that is actually well known: it is stochastic physically-based modeling, which needs to be brought to a new light in hydrology. Here the term "stochastic" is used to collectively represent probability, statistics and stochastic processes.

In the next Section of the paper we take some notes on terminology which also provide 50 the rationale for stochastic physically-based modeling. The third section of the paper is 51 dedicated to the theory underlying the new blueprint that we are proposing. The fourth 52 section describes the practical application of the proposed blueprint. The fifth section 53 reviews the underlying assumptions and their limitations. Open research questions are 54 discussed in the sixth section while the seventh is dedicated to placing existing approaches 55 to uncertainty assessment in hydrology within the new blueprint. Finally we present an 56 example of application and draw some conclusions. 57

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2. Some notes on Terminology

First, let us note that traditionally, the term "physically-based model" is at the same time indicating a "spatially-distributed model" and a "deterministic model". We believe that this is not correct and therefore provide the following clarifications for these terms.

A physically-based model builds on the application of the laws of physics. In view of 61 the extreme complexity, diversity and heterogeneity of meteorologic and hydrological pro-62 cesses (rainfall, soil properties...) physically-based equations are typically (but not neces-63 sarily) applied at local (small spatial) scale, therefore implementing a spatially-distributed 64 representation. Spatial discretization is obtained by subdividing the catchment in sub-65 units (subcatchments, regular grids, or other discretization methods). On the other hand, 66 we may note that a full "reductionist" approach, in which all heterogeneous details of a 67 catchment would be modelled explicitly and the modeling of details would provide the behaviour of the entire system, is a hopeless task [Savenije, 2009]. Indeed, some degree 69 of approximation is unavoidable [Beven, 1989]. 70

In hydrology, the most used physical laws are the gravitation law of Newton and the laws of conservation of mass, energy and momentum. However, it may be useful to make two clarifications, here:

While these laws give simple and meaningful descriptions of problems in simple
 systems, their application in hydrological systems demands simplification, lumping and
 statistical parameterization, and sometimes even replacing by conceptual or statistical
 laws (e.g. the Manning formula. See *Beven* [1989] for an extended discussion).

⁷⁸ 2. Hydrometeorological processes are governed by the laws of thermodynamics, which
⁷⁹ are, au fond, statistical physical laws. In this respect, complex systems cannot be modelled
⁸⁰ without enrolling statistics, as an inextricable part of physics.

These above arguments are usually forgotten and thus physically-based models typically 81 refer to models reducible to Newton's and conservation laws. However, in this case one 82 could conclude that a physically-based model is a delusion: even the simplest hydrological 83 system is not reducible to such simple elements that these laws could be applied in their 84 original form. For these reasons, here we use the term "physically-based model" with a 85 wider content, so as to include some conceptualizations and statistical parameterizations. 86 Furthermore, one may note that a hydrological model should, in addition to be physically-87 based, also consider chemistry, ecology, and so on (see, for instance, Laio [2006], Hopp et 88 al. [2009]). We will focus here on physically-based models only, but the framework that 89 we propose is generally applicable with any type of approach. 90

Many models in hydrology, including the physically-based ones, are often presented in 91 deterministic form. Actually, a deterministic model is one where outcomes are precisely 92 determined through known relationships among states and events, without any room for 93 random variation. In such model, a given input will always produce the same output and 94 therefore uncertainty is not taken into account. This is a relevant limitation, given that 95 uncertainty is always present in hydrological processes, which is not just related to limited 96 knowledge (epistemic uncertainty). It is rather induced, at least in part, by the above 97 mentioned inherent variability and therefore it is unavoidable (see Koutsoyiannis et al. 98 [2009]). It follows that deterministic representation, strictly speaking, is not possible in 99

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¹⁰⁰ catchment hydrology. However, this conclusion does not apply to physica ¹⁰¹ which, in view of our reasoning above, are not necessarily deterministic.

There are many possible alternatives to deal with uncertainty thereby overcoming the 102 limitations of deterministic approaches, including subjective approaches like fuzzy logic, 103 possibility theory, and others [Montanari, 2007]. We believe that one of the most com-104 prehensive ways of dealing with uncertainty is provided by the theory of probability. 105 In fact, probabilistic descriptions allow predictability (supported by deterministic laws) 106 and unpredictability (given by randomness) to coexist in a unified theoretical framework, 107 therefore giving one the means to efficiently exploit and improve the available physical 108 understanding of uncertain systems [Koutsoyiannis et al., 2009]. The theory of stochastic 109 processes also allows the incorporation into our descriptions of (possibly man induced) 110 changes affecting hydrological processes [Koutsoyiannis, 2011], by modifying their physi-111 cal representation and/or their statistical properties (see, for instance, Merz and Blöschl 112 [2008a, b]). Finally, subjectivity and expert knowledge can be taken into account in prior 113 distribution functions through Bayesian theory [Box and Tiao, 1973]. 114

Therefore, a stochastic representation is a valuable opportunity in catchment hydrology, implying that a possible solution to model uncertain systems with a physically-based approach is the above mentioned stochastic physically-based modeling. We formalize the theoretical framework for the application of this type of approach here below.

3. Formulating a Physically-Based Model Within a Stochastic Framework

In this section we show how a deterministic model can be converted into an essential part of a wider stochastic approach through an analytical transformation, by simply introducing a deviation (an error term) from a single-valued relationship. The above

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mentioned analytical transformation is rather technical and is expressed by equations (1) to (6) below. We would like to introduce the new blueprint with a fully comprehensible treatment for those who are not acquainted with (or do not like) statistics. Therefore, the presentation is structured to allow the reader who is interested in the application only to directly jump to equations (7) and (8) without any loss of practical meaning.

Hydrological models are often expressed through a deterministic formulation, namely,
a single valued transformation. In general, it can be written as

$$Q_p = S(\boldsymbol{\epsilon}, \mathbf{I}) \tag{1}$$

where Q_p is the model prediction which, in a deterministic framework, is implicitly assumed to equal the true value of the variable to be predicted. The mathematical relationship *S* represents the model structure, **I** is the input data vector and $\boldsymbol{\epsilon}$ the parameter vector. In the stochastic framework, the hydrological model is expressed in stochastic terms, namely [*Koutsoyiannis*, 2010],

$$f_{Q_p}(Q_p) = K f_{\boldsymbol{\epsilon}, \mathbf{I}}(\boldsymbol{\epsilon}, \mathbf{I})$$
⁽²⁾

where f indicates a probability density function, and K is a transfer operator that depends on deterministic model S. Within this context, Q_p indicates the true variable to be predicted, which is unknown at the prediction time and therefore is treated as a random variable.

Given that a single-valued transformation $S(\boldsymbol{\epsilon}, \mathbf{I})$ as in eq. (1) represents the deterministic part of the hydrological model, the operator K will be similar to the Frobenius-Perron operator (e.g. *Koutsoyiannis* [2010]). However, K can be generalized to represent a so-

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called stochastic operator, which implements a shift from one to many transformations S.

¹⁴⁵ A stochastic operator can be defined by using a stochastic kernel $k(e, \epsilon, \mathbf{I})$, with e¹⁴⁶ reflecting a deviation from a single valued transformation. Let e be a stochastic process, ¹⁴⁷ with marginal probability density $f_e(e)$, representing the global model error according to ¹⁴⁸ the additive relationship

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$$Q_p = S\left(\boldsymbol{\epsilon}, \mathbf{I}\right) + e \;. \tag{3}$$

¹⁵⁰ Note that alternative error structures can be defined, for instance by introducing multi-¹⁵¹ plicative terms. Here the global model error e is defined as the difference between the ¹⁵² true value and the simulation provided by a given model with fixed parameters and input ¹⁵³ data.

¹⁵⁴ The stochastic kernel introduced above must satisfy the following conditions:

$$k(e, \boldsymbol{\epsilon}, \mathbf{I}) \ge 0 \text{ and } \int_{e} k(e, \boldsymbol{\epsilon}, \mathbf{I}) de = 1 ,$$
 (4)

which are met if $k(e, \epsilon, \mathbf{I})$ is a probability density function with respect to e.

¹⁵⁷ Specifically, the operator K applying on $f_{\epsilon,\mathbf{I}}(\epsilon,\mathbf{I})$ is then defined as [Lasota and Mackey, ¹⁵⁸ 1985, p. 101]

$$Kf_{\boldsymbol{\epsilon},\mathbf{I}}\left(\boldsymbol{\epsilon},\mathbf{I}\right) = \int_{\boldsymbol{\epsilon}} \int_{\mathbf{I}} k\left(e,\boldsymbol{\epsilon},\mathbf{I}\right) f_{\boldsymbol{\epsilon},\mathbf{I}}\left(\boldsymbol{\epsilon},\mathbf{I}\right) d\boldsymbol{\epsilon} d\mathbf{I} .$$
(5)

If the vectors of random variables $\boldsymbol{\epsilon}$ and \mathbf{I} are independent to each other (although dependence may be present among the components of each one), the joint probability distribution $f_{\boldsymbol{\epsilon},\mathbf{I}}(\boldsymbol{\epsilon},\mathbf{I})$ can be substituted by the product of the two marginal distributions $f_{\boldsymbol{\epsilon}}(\boldsymbol{\epsilon}) f_{\boldsymbol{I}}(\boldsymbol{I})$. In view of this latter result, by combining eq. (2) and eq. (5), in which the

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X - 10 MONTANARI AND KOUTSOYIANNIS: PHYSICALLY-BASED MODELING OF UNCERTAIN SYSTEMS ¹⁶⁴ model error can be written as $e = Q_p - S(\epsilon, \mathbf{I})$ according to eq. (3), one obtains

$$f_{Q_p}(Q_p) = \int_{\boldsymbol{\epsilon}} \int_{\mathbf{I}} k \left[Q_p - S\left(\boldsymbol{\epsilon}, \mathbf{I}\right), \boldsymbol{\epsilon}, \mathbf{I} \right] f_{\boldsymbol{\epsilon}}\left(\boldsymbol{\epsilon}\right) f_{\mathbf{I}}\left(\mathbf{I}\right) d\boldsymbol{\epsilon} d\mathbf{I} .$$
(6)

At this stage one needs to identify a suitable expression for $k [Q_p - S(\boldsymbol{\epsilon}, \mathbf{I}), \boldsymbol{\epsilon}, \mathbf{I}]$. Upon substituting eq. (3) in eq. (6) and remembering that k is a probability density function with respect to the global model error e, we recognize that the kernel is none other than the conditional density function of e for the given $\boldsymbol{\epsilon}$ and \mathbf{I} , i.e., $f_{e|\boldsymbol{\epsilon},\mathbf{I}} [Q_p - S(\boldsymbol{\epsilon},\mathbf{I})|\boldsymbol{\epsilon},\mathbf{I}]$. To summarise the whole set of analytical derivations expressed by equations (1) to (6) one may conclude that we passed from the deterministic formulation of the hydrological model expressed by eq. (1), which we replicate for clarity here below,

$$Q_p = S\left(\boldsymbol{\epsilon}, \mathbf{I}\right) \tag{7}$$

¹⁷⁴ to the stochastic formulation expressed by

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$$f_{Q_p}(Q_p) = \int_{\boldsymbol{\epsilon}} \int_{\mathbf{I}} f_{e|\boldsymbol{\epsilon},\mathbf{I}} \left[Q_p - S\left(\boldsymbol{\epsilon},\mathbf{I}\right) | \boldsymbol{\epsilon},\mathbf{I} \right] f_{\boldsymbol{\epsilon}}\left(\boldsymbol{\epsilon}\right) f_{\mathbf{I}}\left(\mathbf{I}\right) d\boldsymbol{\epsilon} d\mathbf{I}$$
(8)

¹⁷⁶ with the following meaning of the symbols:

¹⁷⁷ - $f_{Q_p}(Q_p)$: probability density function of the true value of the hydrological variable to ¹⁷⁸ be predicted;

179 - $S(\boldsymbol{\epsilon}, \mathbf{I})$: deterministic part of the hydrological model;

¹⁸⁰ - $f_{e|\epsilon,\mathbf{I}}[Q_p - S(\epsilon,\mathbf{I})|\epsilon,\mathbf{I}]$: conditional probability density function of the global model ¹⁸¹ error. According to eq. 2 it can also be written as $f_{e|\epsilon,\mathbf{I}}(e|\epsilon,\mathbf{I})$;

- ¹⁸² ϵ : model parameter vector;
- 183 $f_{\epsilon}(\epsilon)$: probability density function of model parameter vector;
- ¹⁸⁴ I: input data vector;
- $_{185}$ $f_{\mathbf{I}}(\mathbf{I})$: probability density function of input data vector.

In eq. (8) the conditional probability distribution of the global model error $f_{e|\epsilon,\mathbf{I}}[Q_p - S(\epsilon,\mathbf{I})|\epsilon,\mathbf{I}]$ is conditioned on the input data vector \mathbf{I} and the parameter vector ϵ . Such formulation would be useful if one needed to account for changes in time of the conditional statistics of the model error (like, for instance, those originated by heteroscedasticity). On the other hand, if one assumed that the global model error is independent of \mathbf{I} and ϵ , then eq. (8) can be written in the simplified form

$$f_{Q_p}(Q_p) = \int_{\boldsymbol{\epsilon}} \int_{\mathbf{I}} f_e \left[Q_p - S\left(\boldsymbol{\epsilon}, \mathbf{I}\right) \right] f_{\boldsymbol{\epsilon}}\left(\boldsymbol{\epsilon}\right) f_{\mathbf{I}}\left(\mathbf{I}\right) d\boldsymbol{\epsilon} d\mathbf{I} .$$
(9)

We anticipate that one of the key issues is to efficiently represent the statistical properties of the global model error, as many contributions proposed by the hydrological literature already pointed out (see, for instance, *Refsgaard et al.* [2006]; *Kuczera et al.* [2006]; *Beven* [2006]).

The presence of a double integral in eq. (8) and eq. (9) may induce the feeling in the reader that the practical application of the proposed framework is cumbersome. Actually, the double integral can be easily computed through numerical integration, namely, by applying a Monte Carlo simulation procedure that is well known and already used in hydrology (see *Koutsoyiannis* [2010]). We explain the numerical integration in the next section of the paper.

4. Application of the Proposed Framework: Joining Hydrological Model Implementation and Uncertainty Assessment

Estimating the probability distribution of the true value of the variable to predicted by a hydrological model is equivalent to simultaneously carry out model implementation and uncertainty assessment. The framework for estimating the probability density function of

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model prediction, $f_{Q_p}(Q_p)$, was proposed in Section 3. Here we show how eq. (8) can be applied in practice.

Let us admit that the hydrological model is fully generic and possibly physically-based. Also, let us admit that the probability density functions of model parameters, input data and model error are known, for instance because they were already estimated by using procedures that were proposed by the hydrological literature (see, for instance, *Di Baldassarre and Montanari* [2009] for input data uncertainty, *Vrugt et al.* [2007] for parameter uncertainty and *Montanari and Brath* [2004] for global model error). A practical demonstration showing how this can be determined is contained in Section 8 below.

²¹⁵ Under the above circumstances the double integral in eq. (8) can be easily computed ²¹⁶ through a Monte Carlo simulation procedure, which can be carried out in practice by ²¹⁷ performing many implementations of the deterministic hydrological model $S(\boldsymbol{\epsilon}, \mathbf{I})$.

²¹⁸ In detail the simulation procedure is carried out through the following steps:

²¹⁹ 1. A parameter vector for the hydrological model is picked up at random from the ²²⁰ model parameter space according to the probability distribution $f_{\epsilon}(\epsilon)$.

221 2. An input data vector for the hydrological model is picked up at random from the 222 input data space according to the probability distribution $f_{\mathbf{I}}(\mathbf{I})$.

3. The hydrological model is run and a model prediction (or a vector of individual predictions) $S(\boldsymbol{\epsilon}, \mathbf{I})$ is computed.

4. A number *n* of realizations of the global model error (or vectors of individual errors) is picked up at random from the model error space according to the probability distribution $f_{e|\epsilon,\mathbf{I}}(e)$ and added to the model prediction $S(\epsilon,\mathbf{I})$.

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5. The simulation described by items from 1 to 4 is repeated j times. Therefore one obtains $n \cdot j$ (vectors of) realizations of the true variable to be predicted Q_p .

6. Finally the probability distribution $f_{Q_p}(Q_p)$ is inferred through the realizations mentioned in item 5.

It is important to note that j needs to be sufficiently large, in order to accurately 232 estimate the probability density $f_{Q_p}(Q_p)$. It is also clarified that in a typical Monte Carlo 233 procedure one would use n = 1 (where, to each simulation a different realisation of model 234 error e would be generated). However, a larger n value multiplies the number of simulated 235 points by a factor n with negligible increase of computer time (as the same hydrological 236 simulation run is used for all n). We believe that a modest value of n (see application in 237 Section 8) results in a good compromise of accuracy and computational efficiency. Figure 238 1 shows a flowchart of the whole simulation procedure. 239

Once the probability distribution of the true value to be predicted Q_p is known the problems of hydrological modeling and uncertainty assessment are both solved.

5. Discussion of the Underlying Assumptions

Like any scientific method, the blueprint proposed in Section 3 and 4 is based on as-242 sumptions in order to ensure applicability. When dealing with uncertainty assessment in 243 hydrology, assumptions are often treated with suspect, because it is felt that they un-244 dermine the effectiveness of the method and therefore its efficiency and credibility with 245 respect to users. We must admit, though, that assumptions are unavoidably needed to set 246 up models, calibrate their parameters and estimate their reliability, whatever approach is 247 used. Evidently, flawed assumptions may falsify statistical inference as well as any alterna-248 tive model of uncertain and deterministic systems. Therefore the target of the researcher 249

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should not be to avoid assumptions, but rather discuss them transparently, evaluate their
effects and, when possible, check them, for instance through statistical testing.

In order to discuss the assumptions conditioning the blueprint we introduced above, 252 first note that the theoretical scheme is very general. In fact, we only assumed that model 253 input data and parameters are random vectors which are independent to each other. Such 254 assumption implies that parameter uncertainty is independent of data uncertainty and its 255 influence on the results depends on data uncertainty itself. Unless this latter is very sig-256 nificant, we believe the assumption is reasonable. In principle the above assumption could 257 be removed by estimating the joint probability distribution of input data and parameters 258 and then picking up from this distribution the random outcomes at steps 1 and 2 of the 259 simulation procedure described in Section 4. Actually, statistical inference of joint prob-260 ability distributions of model input data and parameters is likely to be affected by much 261 uncertainty and therefore it may be more difficult to implement. We plan to study this 262 solution in future research. 263

One may note that further assumptions might be needed to estimate the probability 264 distribution f_e of model error, which might be non-Gaussian and affected by heteroscedas-265 ticity. For instance, in the application presented in Section 8 the meta-Gaussian approach 266 by Montanari and Brath [2004] is applied. Actually, this method assumes that the joint 267 probability distribution of model error and model simulation is stationary and independent 268 of input uncertainty and parameter uncertainty, but the marginal probability distribution 269 of the model error can eventually result heteroscedastic (see Section 8 and Montanari and 270 Brath [2004]). If one used the Generalised Likelihood Uncertainty Estimation (GLUE; 271 see Beven and Binley [1992]) different assumptions would be introduced depending on 272

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²⁷³ the (possibly informal) likelihood measure that is used to characterise the reliability of ²⁷⁴ model output. No matter which method is used, any additional assumption introduced ²⁷⁵ for inferring f_e should be appropriately checked.

A relevant issue has been pointed out by some authors (see, for instance, Beven et al. 276 [2011]) who are convinced that epistemic errors arising from hydrological models might 277 be affected by non-stationarity and therefore difficult (or impossible) to model by using 278 statistical approaches. In our opinion epistemic uncertainty in itself, which is not chang-279 ing in time, cannot induce non-stationarity, which might instead be necessary to enrol 280 when environmental changes are present. However, independently from its origin, non-281 stationarity can be efficiently dealt with by using non-stationary stochastic processes, by 282 introducing and checking suitable assumptions. 283

The conclusion of the above discussion can be summarised by saying that (a) the only 284 relevant assumption conditioning the proposed blueprint is justified as long as data un-285 certainty is not very significant (see also additional discussion about this in Section 8.3). 286 Within this respect, we would like to emphasise our opinion that in the presence of signifi-287 cant input data errors (also called "observation uncertainty") any uncertainty assessment 288 method is ill-posed and likely to end up with underestimation. Moreover, (b) the above 289 assumption can in principle be removed although it is likely that this option turns out 290 to be more difficult to handle in practice. And finally, (c) further assumptions might be 291 needed for ensuring the practical application of the approach, which should be appropri-292 ately checked. 293

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6. Open Research Questions

The above discourse shows that to include a deterministic model within a stochastic 294 framework is in principle possible. Although we explicitly focused on physically-based 295 approaches, the blueprint that we are proposing is applicable to any deterministic scheme, 296 therefore including conceptual and black-box models. We believe that incorporation of 297 physically-based deterministic models bears a greater added value of the blueprint we are 298 proposing. In fact, analyzing the randomness of physically-based systems is an invaluable 299 opportunity to improve their understanding therefore increasing predictability, according 300 to the "models of everywhere" concept [Beven, 2007]. 301

However, relevant research challenges and practical problems may prevent a successful application of the blueprint. First of all, numerical integration (e.g. the Monte Carlo simulation outlined in Section 4) is computationally intensive and may result prohibitive for spatially-distributed models. Therefore efficient simulation schemes are necessary, while too detailed spatial representations may not make any difference except in wasting computer time.

Second, a relevant issue is the estimation of global model uncertainty, namely, the 308 estimation of the probability distribution $f_e(e)$ of the model error. The literature has 309 proposed a variety of different approaches, like the above mentioned GLUE method [Beven 310 and Binley, 1992, the meta-Gaussian model [Montanari and Brath, 2004; Montanari and 311 Grossi, 2008], Bayesian Model Averaging (BMA, Neuman [2003]) and BATEA [Kuczera 312 et al., 2006. However, the above methods rely on limiting assumptions and some of 313 them are too computer intensive. We believe that estimating global model uncertainty in 314 hydrology [Montanari, 2011] is still an open problem for which more focused research is 315

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Finally, estimation of parameter uncertainty is a relevant challenge as well. Possibilities are the GLUE method [*Beven and Binley*, 1992] and the DREAM algorithm [*Vrugt et al.*, 2007], which nevertheless are computer intensive as well and may turn out to be inpractical with spatially-distributed models applied to fine time scale at large catchments.

7. Placing Uncertainty Assessment Techniques Within the Proposed Blueprint

The blueprint proposed in Section 3 and 4 aims to provide a general theoretical frame-322 work for uncertainty assessment in hydrology. Indeed, the most frequently used techniques 323 can be easily placed within it. For instance, the well known GLUE method Beven and 324 *Binley*, 1992 anticipated many of the concepts we are highlighting here, and in particular 325 the idea of estimating uncertainty by turning from one to many applications of the hydro-326 logical model. In detail, the simulation procedure used within the classical applications 327 of GLUE is much similar to what is presented in Section 4. The only relevant differ-328 ence is related to the estimation of global model error, which is resolved within GLUE 329 by estimating the model likelihood, and therefore the probability distribution of the true 330 variable to be predicted, through an integral performance measure or by fixing limits of 331 acceptability [Liu et al., 2009; Winsemius et al., 2009]. In fact, likelihood is estimated 332 within classical GLUE by adopting an informal approach, basing on a dummy likelihood 333 measure (like the Nash-Sutcliffe efficiency in many GLUE applications). Basing on the 334 blueprint proposed here, GLUE can then be defined as a statistical approach where model 335 likelihood is estimated informally. 336

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³³⁷ Moreover, the proposed blueprint reduces to the meta-Gaussian approach by *Montanari* ³³⁸ and Brath [2004], once that parameter uncertainty and input uncertainty are neglected. ³³⁹ A similar reasoning applies to the Bayesian Forecasting System by *Krzysztofowicz* [2002], ³⁴⁰ where parameter uncertainty is neglected and the probability distribution of the true ³⁴¹ variable to be predicted is estimated by inferring the joint probability distribution of true ³⁴² value and corresponding model output.

8. An Example of Application

In order to illustrate the proposed blueprint with a practical example, an application is presented here below that refers to a rainfall-runoff model applied to a catchment located in Italy.

8.1. The study catchment

The application refers to the Leo River at Fanano, in the Emilia-Romagna region, in Northern Italy. Figure 2 shows the location of the catchment. The catchment area is 64.4 km² and the main stream length is about 10 km. The maximum elevation in the catchment is the Mount Cimone (2165 m a.s.l.), which is the highest peak in the northern part of the Apennine Mountains. The climate over the region is continental.

Daily river flow data at Fanano are available for the period January 1st, 2003 - October 26th, 2008, for a total of 2126 observations. For the same period, daily mean areal rainfall and temperature data over the catchment are available, as estimated by the Italian National Hydrographic Service basing on observation collected in nearby gauging stations. The observations collected from January 1st 2003 to December 31st 2007 were used for calibrating the rainfall-runoff model, while the period September 1st 2007 - October

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³⁵⁷ 26th 2008 was reserved for its validation. We estimated the probability distribution of ³⁵⁸ the model error by referring to the first year of the validation period (2007), in order ³⁵⁹ to obtain a reliable assessment of $f_{e|\epsilon,\mathbf{I}}(e|\epsilon,\mathbf{I})$ in a real world application. Note that the ³⁶⁰ general formulation of eq. (8) is used, thereby accounting for heteroscedasticity in the ³⁶¹ model error itself. Finally, the period January 1st 2008 - October 26th 2008 was reserved ³⁶² for testing, in full validation mode, the proposed blueprint (rainfall-runoff modeling and ³⁶³ uncertainty assessment).

8.2. The rainfall-runoff model

The rainfall-runoff model is AFFDEF [Moretti and Montanari, 2007], a spatially-364 distributed grid-based approach where hydrological processes are described with 365 physically-based and conceptual equations. In order to limit the computational require-366 ments, and in view of the limited catchment area, the Leo river basin was described 367 by using only one grid cell, therefore applying a lumped representation. AFFDEF was 368 calibrated by using DREAM [Vrugt et al., 2007], that is, a modified SCEM-UA global 369 optimisation algorithm [Vrugt et al., 2003]. The DREAM method makes use of popula-370 tion evolution like a genetic algorithm together with a selection rule to assess whether a 371 candidate parameter set is to be retained. The sample of retained sets after convergence 372 can be used to infer the probability distribution of model parameters. Herein, a number 373 of 1000 parameter sets were retained, which indirectly determine the density function 374 $f_{\epsilon}(\epsilon)$ of the parameter vector in a non-parametric empirical manner, fully respecting the 375 dependencies between different parameters. 376

AFFDEF explained about 57% and 50% of the river flow variance in calibration and validation, respectively. Figure 3 reports a comparison during the validation period (2007

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and 2008) between observed and simulated hydrographs. This latter was obtained by using the best parameter set according to explained variance during the calibration period. One can see that a significant uncertainty affects the model performances, which is unlikely merely due to lumping the model at catchment scale. We are interested in checking whether the proposed blueprint provides a consistent assessment of such uncertainty.

Finally, the probability distribution of the model error was inferred by using the meta-384 Gaussian approach by Montanari and Brath [2004]. In brief, the method recognizes that 385 the error is affected by heteroscedasticiticy by accounting for the dependence of its condi-386 tional probability distribution on model prediction. In this way change of the statistical 387 properties during time is efficiently modeled. The estimation of the joint probability dis-388 tribution of model simulation (provided by AFFDEF by using the best parameter set 389 in terms of explained variance during the calibration period) and error is carried out 390 by preliminarily transforming the data to the Gaussian probability distribution. In the 391 Gaussian domain a bivariate Gaussian distribution is finally estimated. The goodness-392 of-fit provided by the meta-Gaussian approach was checked by using the statistical tests 393 described in *Montanari and Brath* [2004], where more details on the procedure can be 394 found. 395

8.3. The simulation procedure

We assumed to neglect input data uncertainty because no information was available to infer the probability distribution of the available observations. This is an important limitation in many practical applications. In particular, input uncertainty is usually dominant in real time flash-flood forecasting, where input rainfall to a rainfall-runoff model is usually predicted to increase the lead time of the river flow forecasting. If a

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⁴⁰¹ probabilistic prediction for rainfall is available then input uncertainty can be efficiently ⁴⁰² taken into account in the blueprint proposed above. In alternative, input uncertainty can ⁴⁰³ be estimated by using expert knowledge or Bayesian procedures like BATEA [*Kuczera et* ⁴⁰⁴ *al.*, 2006]. Given that the present application refers to a past period and excludes future ⁴⁰⁵ forecast inputs, and since data series have been tested, it is reasonable to assume data ⁴⁰⁶ certainty, with the awareness that we may slightly underestimate prediction uncertainty ⁴⁰⁷ in this case.

The simulation procedure was performed by running AFFDEF during the 300-day val-408 idation period January 1st 2008 - October 26, 2008, for each of the j = 1000 parameter 409 sets retained by DREAM. Then, n = 100 random outcomes from the probability distribu-410 tion of the model error were added to each observation of the 1000 simulated data series, 411 therefore obtaining $1000 \cdot 100$ simulations of the data value referred to each of the above 412 300 days, which allowed us to estimate the related probability distribution. The above 413 j and n values were selected by estimating the number of sampling points to efficiently 414 infer the shape of the related probability distributions. 415

Figure 4 shows the 95% confidence band of the model simulation, along with the corresponding observations. It can be seen that the results are physically meaningful and, in our opinion, confirm the efficiency of the proposed blueprint. In fact, the confidence bands are quite large as one would expect by looking at the performances of the model, which underline the presence of significant uncertainty. A number of data points are located outside the confidence bands as one would expect by considering that the band itself is drawn at the 95% confidence level.

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9. Conclusions

A new blueprint is presented for formulating physically-based models of uncertain hydrological systems, which in effect means all hydrological systems. The main advantages of the proposed methodological scheme are that (a) hydrological modeling and uncertainty assessment are jointly carried out and (b) a general theoretical framework is elaborated for uncertainty estimation in hydrology, which includes as special cases the existing and most frequently used methods.

Basically, the blueprint proposes to incorporate deterministic hydrological models within 429 a stochastic framework. This solution is suggested by our convincement that probability 430 is the most efficient and objective technique for uncertainty assessment. Shifting from the 431 deterministic to the stochastic formulation requires passing from one to many applications 432 of the hydrological model. What we suggest is not new in practical applications and con-433 stitutes also the rationale underlying some of the existing uncertainty assessment methods 434 like GLUE [Beven and Binley, 1992]. However, a comprehensive theoretical framework 435 is proposed, along with a detailed discussion of the underlying assumptions, therefore 436 allowing one to structure in a objective setting the application of hydrological models in 437 order for uncertainty to be taken into account and estimated. 438

An application to an Italian river basin is presented for illustrating the introduced blueprint. Although a simplifying assumption was introduced to neglect data uncertainty and a lumped rainfall-runoff model was used, the case study shows that the proposed approach is efficient and physically meaningful.

We believe the theoretical framework introduced here may open new perspectives regarding modeling of uncertain hydrological systems. In fact, statistical analysis of un-

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⁴⁴⁵ certainty and predictability offers valuable indications to improve our understanding of
⁴⁴⁶ real systems and better understand their (possibly) changing or shifting behaviors and
⁴⁴⁷ their reaction to (human induced) changes. Last but not least, we believe that the pro⁴⁴⁸ posed procedure is very useful for educational purposes, putting the basis for developing
⁴⁴⁹ a unified theoretical basis for uncertainty assessment in hydrology.

Relevant research questions are still open. The proposed procedure is based on running multiple simulations and therefore it is computationally intensive. For this reason, application to very detailed spatial representation implemented on complex systems may require significant computational resources. Finally, estimation of parameter uncertainty, global model uncertainty and data uncertainty may represent relevant problems for some real world applications, for which additional and focused research is needed.

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Figure 1. Flowchart of the Monte Carlo simulation procedure for performing the numerical integration in eq. (8). The marginal distribution f_e is replaced by the conditional $f_{e|\epsilon,\mathbf{I}}$ when the error depends on parameters and inputs.



Figure 2. Location of the Leo River basin (Italy).

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Figure 3. Comparison between observed and simulated hydrographs during the validation period (Jan 1st 2007 - October 26, 2008). The simulated hydrograph was obtained by using the best parameter set according to explained variance during the calibration period.



Figure 4. 95% confidence bands of the river flow simulation provided by AFFDEF during the validation period (Jan 1st, 2008 - Oct 26th, 2008) of the proposed blueprint, along with the corresponding observed values.

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